

Fig. 1. Variation of the local values of normalized R indices as a function of y_i for different fixed values of σ_i^2 . For the definition of $R_1(y)$, $R_1(z)$, etc., see column 6 of Table 1.

P/N . (iii) Divide the range $0 \leq s \leq S_{\max}$ into a number of narrow subintervals. Determine from the data the number (n_s) of observed reflections in each of these sub-intervals. (iv) From the mean value of $\sin \theta/\lambda$ corresponding to each sub-interval determine the values of f . (v) Calculate σ_A (by taking $\langle |\Delta r| \rangle = 0.2 \text{ \AA}$) corresponding to each of these sub-intervals. (vi) Make use of the results in Tables 2–4 and determine the values of $[R]_i$ for these sub-intervals by bilinear interpolation. (vii) Make use of the results thus obtained in the appropriate expressions for $[\bar{R}]_i$ and compute the overall values $[\bar{R}]_i$. The values thus obtained represent the theoretical overall values of the normalized R indices corresponding to a model for which $\langle |\Delta r| \rangle = 0.2 \text{ \AA}$ and for data in which $y_N \geq y_i$ and $0 \leq s \leq S_{\max}$.

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Theoretical Evaluation of the Overall Values of Discrepancy Indices for Truncated Data. II. Normalized R indices for a Non-centrosymmetric Crystal with Similar Atoms

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Abstract

Theoretical expressions and numerical tables for the local values of six types of normalized R indices are obtained for an imperfectly related incomplete model of

a non-centrosymmetric crystal with truncated data. Under similar conditions, the curve of the local value of an R index *versus* the truncation limit y_i is relatively more flat for the non-centrosymmetric case than for the centrosymmetric case particularly in the region where y_i is small.

* Contribution No. 546.

1. Introduction

In part I (Parthasarathy & Velmurugan, 1981), we derived the theoretical expressions necessary for calculating the overall values of various normalized R indices for a C crystal with truncated data. In this paper we shall derive the corresponding results applicable to an NC crystal. The notation used here is the same as in part I. Since the method of derivation closely follows that used in part I, we shall give only the essential steps.

2. Derivation of the theoretical expressions for the normalized R indices

2.1. Derivation of the joint p.d.f. of y_N and y_P^c for the truncated data

The joint p.d.f. of y_N and y_P^c for the NC case is known to be (SP, 1976)

$$P(y_N, y_P^c) = \frac{4y_N y_P^c}{\sigma_B^2} \exp\left[-\frac{(y_N^2 + (y_P^c)^2)}{\sigma_B^2}\right] \times I_0\left(\frac{2\sigma_A y_N y_P^c}{\sigma_B^2}\right), \quad 0 \leq y_N < \infty, 0 \leq y_P^c < \infty, \quad (1)$$

The joint p.d.f. of y_N and y_P^c applicable to the truncated data will therefore be given by [see (13) and (14) of part I]

$$P_t(y_N, y_P^c) = \frac{4y_N y_P^c}{\sigma_B^2 \beta_{NC}} \exp\left[-\frac{[y_N^2 + (y_P^c)^2]}{\sigma_B^2}\right] \times I_0\left(\frac{2\sigma_A y_N y_P^c}{\sigma_B^2}\right), \quad (2)$$

where β_{NC} can be shown to be [see equation (A-5) of the Appendix*]

$$\beta_{NC} = \exp(-y_i^2). \quad (3)$$

2.2. Derivation of the theoretical expressions for the normalized R indices

Index $[R_1(y)]_t$. Equation (21) of part I is valid for this case as well except that β_C is now to be replaced by β_{NC} . Since the first term within the square brackets represents $R_1(y)$ (see §2.3 of part I), and since

$\langle y_N \rangle = \sqrt{\pi}/2$ for the NC case (Wilson, 1949), we obtain

$$[R_1(y)]_t = \left[R_1(y) - \frac{2}{\sqrt{\pi}} \int_0^{y/(1+y)} \int_0^1 \left| \frac{u}{1-u} - \frac{v}{1-v} \right| \times P\left(\frac{u}{1-u}, \frac{v}{1-v}\right) \frac{du dv}{(1-u)^2(1-v)^2} \right] \times [2\pi^{-1/2} \beta_{NC} y_t + \operatorname{erfc}(y)]^{-1} \quad (4)$$

where we have used (A-7) of part II and the substitution in (24) of part I. $R_1(y)$ is known to be (Srinivasan & Parthasarathy, 1976; hereafter SP, 1976)

$$R_1(y) = \frac{3\sigma_B^3}{2} \int_0^1 \frac{{}_2F_1(-\frac{1}{4}, -\frac{3}{4}; 1; \sigma_A^2 x^2) dx}{(1+x)^{1/2} (1-\sigma_A^2 x^2)^2}. \quad (5)$$

Index $[R_1(z)]_t$. Equation (26) of part I is valid for this case as well. Using (A-11) and following the steps used for the C case, we obtain

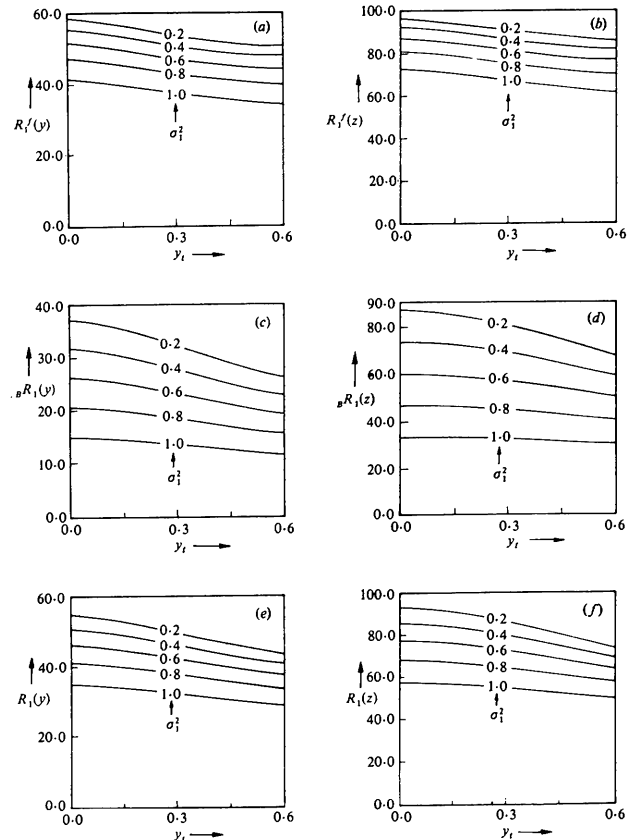


Fig. 1. Variation of the local values of normalized R indices as a function of y_i for different fixed values of σ_i^2 . For the definition of $R_1(y)$, $R_1(z)$, etc., see column 6 of Table 1 of part I.

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$$[R_1(z)]_t = \left[R_1(z) - \int_0^{y/(1+y)} \int_0^1 \left| \left(\frac{u}{1-u} \right)^2 - \left(\frac{v}{1-v} \right)^2 \right| \times P \left(\frac{u}{1-u}, \frac{v}{1-v} \right) \frac{du dv}{(1-u)^2 (1-v)^2} \right] \times [\beta_{NC}(1+y^2)]^{-1}, \quad (6)$$

where $R_1(z)$ has been shown to be (SP, 1976)

$$R_1(z) = \sigma_B. \quad (7)$$

Index $[_B R_1(y)]_t$. Equation (30) of part I is valid for this case as well. Substituting for $\langle y_N^2 \rangle_t$, $\langle (y^2)^2 \rangle_t$ and $\langle y_N y_N^2 \rangle_t$ from (A-11), (A-14) and (A-16) respectively in

equation (30) of part I and simplifying the result, we obtain

$$[_B R_1(y)]_t = \left\{ {}_B R_1(y) + 2(\beta_{NC} - 1) + \beta_{NC} y_t^2 (1 + \sigma_A^2) + \frac{\sqrt{\pi}}{\sigma_B} \int_0^{y_t} u^{1/2} \exp[-u(1 + \sigma_B^2)/2\sigma_B^2] \times \left[(\sigma_B^2 + \sigma_A^2 u) I_0 \left(\frac{\sigma_A^2 u}{2\sigma_B^2} \right) + \sigma_A^2 u I_1 \left(\frac{\sigma_A^2 u}{2\sigma_B^2} \right) \right] du \right\} \times [\beta_{NC}(1+y^2)]^{-1}, \quad (8)$$

where ${}_B R_1(y)$ is known to be (SP, 1976)

Table 1. Values of $[R_1(y)]_t$ and $[R_1(z)]_t$ as functions of σ_A and y_t for the non-centrosymmetric case

$\sigma_A \rightarrow$		$[R_1(y)]_t$					$[R_1(z)]_t$					
$y_t \rightarrow$		0.00	0.15	0.30	0.45	0.60	$y_t \rightarrow$	0.00	0.15	0.30	0.45	0.60
0.000		58.579	56.744	52.846	48.833	45.841	100.000	97.824	92.103	84.755	77.772	
0.040		58.536	56.703	52.809	48.801	45.813	99.920	97.747	92.036	84.700	77.728	
0.080		58.409	56.581	52.699	48.705	45.729	99.679	97.517	91.834	84.535	77.598	
0.120		58.219	56.387	52.524	48.546	45.588	99.477	97.133	91.496	84.258	77.380	
0.160		57.985	56.127	52.287	48.320	45.490	99.312	96.592	91.021	83.869	77.071	
0.200		57.505	55.712	51.918	48.028	45.132	97.980	95.891	90.404	83.363	76.668	
0.240		57.024	55.250	51.502	47.667	44.813	97.077	95.027	89.643	82.736	76.168	
0.280		56.449	54.697	51.004	47.234	44.429	96.000	93.995	88.733	81.985	75.566	
0.320		55.776	54.050	50.422	46.727	43.978	94.742	92.790	87.668	81.103	74.854	
0.360		55.000	53.304	49.749	46.140	43.555	93.295	91.403	86.439	80.082	74.024	
0.400		54.116	52.454	48.993	45.470	43.155	91.652	89.825	85.040	78.913	72.401	
0.420		53.833	52.188	48.852	45.102	42.854	90.872	89.272	84.472	78.582	72.182	
0.440		53.517	51.849	48.515	44.710	42.571	89.800	88.047	83.454	77.453	71.494	
0.460		53.257	51.568	48.164	44.294	42.306	88.792	87.079	82.594	76.457	70.675	
0.480		53.049	51.322	47.819	43.853	42.058	87.727	86.055	81.679	75.604	70.072	
0.500		52.882	51.100	47.608	43.585	41.917	86.603	84.973	80.712	75.208	70.025	
0.520		52.757	50.903	47.424	43.389	41.789	85.417	83.828	79.689	74.394	69.306	
0.540		52.675	50.734	47.264	43.254	41.672	84.167	82.632	78.609	73.441	68.526	
0.560		52.626	50.595	47.128	43.180	41.565	82.859	81.359	77.467	72.494	67.699	
0.580		52.607	50.484	47.015	43.159	41.465	81.462	80.021	76.262	71.457	66.808	
0.600		52.614	50.400	46.924	43.084	41.372	80.000	78.611	74.989	70.358	65.863	
0.610		52.630	50.341	46.853	43.039	41.312	79.240	77.878	74.325	69.702	65.337	
0.620		52.656	50.297	46.801	43.000	41.264	78.460	77.125	73.643	69.124	64.855	
0.630		52.692	50.266	46.764	42.974	41.230	77.660	76.351	72.942	68.582	64.325	
0.640		52.738	50.245	46.740	42.950	41.206	76.837	75.527	72.221	67.921	63.778	
0.650		52.794	50.232	46.726	42.936	41.191	76.000	74.700	71.490	67.207	63.215	
0.660		52.860	50.226	46.720	42.930	41.184	75.127	73.903	71.171	66.639	62.627	
0.670		52.936	50.226	46.720	42.930	41.184	74.236	73.041	69.932	65.951	62.022	
0.680		53.022	50.231	46.722	42.932	41.186	73.321	72.156	69.124	65.240	61.395	
0.690		53.118	50.240	46.726	42.936	41.190	72.381	71.245	68.293	64.507	60.745	
0.700		53.224	50.253	46.732	42.942	41.196	71.414	70.309	67.436	63.750	60.075	
0.710		53.340	50.270	46.740	42.950	41.204	70.426	69.346	66.524	62.980	59.375	
0.720		53.466	50.290	46.750	42.960	41.214	69.377	68.354	65.544	62.180	58.657	
0.730		53.602	50.314	46.762	42.972	41.226	68.345	67.333	64.706	61.325	57.908	
0.740		53.748	50.344	46.776	42.986	41.240	67.261	66.281	63.738	60.460	57.131	
0.750		53.904	50.380	46.792	42.992	41.256	66.144	65.197	62.739	59.565	56.322	
0.760		54.070	50.422	46.810	43.000	41.272	65.000	64.078	61.706	58.638	55.484	
0.770		54.246	50.470	46.830	43.010	41.290	63.804	62.924	60.639	57.676	54.611	
0.780		54.432	50.524	46.852	43.022	41.310	62.578	61.731	59.534	56.678	53.702	
0.790		54.628	50.584	46.876	43.036	41.332	61.311	60.498	58.390	55.642	52.755	
0.800		54.834	50.650	46.902	43.052	41.356	60.000	59.222	57.204	54.564	51.766	
0.810		55.050	50.722	46.930	43.070	41.382	58.643	57.900	55.973	53.441	50.730	
0.820		55.276	50.800	46.960	43.090	41.410	57.236	56.529	56.493	52.271	49.654	
0.830		55.512	50.884	47.000	43.112	41.440	55.876	55.105	55.362	51.049	48.524	
0.840		55.758	50.974	47.042	43.136	41.472	54.529	53.623	54.173	49.771	47.357	
0.850		56.014	51.070	47.088	43.162	41.506	53.196	52.079	52.924	48.431	46.090	
0.860		56.280	51.172	47.134	43.190	41.542	51.878	50.468	51.617	47.025	44.777	
0.870		56.556	51.280	47.182	43.220	41.580	50.575	49.007	49.907	45.544	43.391	
0.880		56.842	51.394	47.232	43.252	41.620	49.305	47.811	47.912	44.016	41.923	
0.890		57.138	51.514	47.286	43.286	41.662	48.087	46.497	46.246	42.441	40.464	
0.900		57.444	51.640	47.342	43.322	41.706	46.924	45.148	44.975	40.975	39.016	
0.910		57.760	51.772	47.400	43.360	41.752	45.818	43.889	43.683	39.677	37.693	
0.920		58.086	51.910	47.460	43.400	41.800	44.764	42.662	42.433	38.454	36.424	
0.930		58.422	52.054	47.522	43.442	41.846	43.746	41.496	41.224	37.254	35.204	
0.940		58.768	52.204	47.586	43.486	41.894	42.774	40.300	40.076	36.114	34.034	
0.950		59.124	52.360	47.652	43.532	41.944	41.848	39.300	38.926	35.004	32.914	
0.955		59.296	52.416	47.676	43.556	41.968	41.724	39.184	38.784	34.884	32.794	
0.960		59.472	52.472	47.700	43.580	41.992	41.600	39.064	38.644	34.764	32.674	
0.965		59.652	52.528	47.724	43.604	42.016	41.476	38.944	38.504	34.644	32.554	
0.970		59.836	52.584	47.748	43.628	42.040	41.352	38.824	38.364	34.524	32.434	
0.975		60.024	52.640	47.772	43.652	42.064	41.228	38.704	38.224	34.404	32.314	
0.980		60.216	52.696	47.796	43.676	42.088	41.104	38.584	38.084	34.284	32.194	
0.985		60.412	52.752	47.820	43.700	42.112	40.980	38.464	37.944	34.164	32.074	
0.990		60.612	52.808	47.844	43.724	42.136	40.856	38.344	37.804	34.044	31.954	
0.995		60.816	52.864	47.868	43.748	42.160	40.732	38.224	37.664	33.924	31.834	
1.000		61.024	52.920	47.892	43.772	42.184	40.608	38.104	37.524	33.804	31.714	

$${}_B R_1(y) = 2 - 2 \left[E(\sigma_A) - \frac{\sigma_B^2}{2} K(\sigma_A) \right]. \quad (9)$$

Index $[_B R_1(z)]_t$. Equation (33) of part I is valid for this case as well. Substituting for $\langle y_N^4 \rangle_t$, $\langle y_N^6 \rangle_t$ and $\langle y_N^8 \rangle_t$ from (A-13), (A-15) and (A-17) respectively and simplifying the result by using (16) of part I, we obtain

$$[_B R_1(z)]_t = \frac{({}_B R_1(z) + \sigma_B^2 + 2\sigma_A^2 \sigma_B^2 y_t^2 + \sigma_B^4 y_t^4)}{(y_t^4 + 2y_t^2 + 2)}, \quad (10)$$

where ${}_B R_1(z)$ is known to be (SP, 1976)

$${}_B R_1(z) = \sigma_B^2. \quad (11)$$

Index $[R_1^f(y)]_t$. Equation (37) of part I is valid for this case as well, provided β_C is replaced by β_{NC} and

$P(y_N, y_N^c)$ is taken to be the function in (1) of this part. Following the method used for this index in part I, the final expression can be shown to be

$$[R_1^f(y)]_t = \frac{1}{\beta_{NC}} \left[R_1^f(y) - 2 \int_0^{y_t/(1+y_t)} \int_0^1 \left| \left[\left(\frac{u}{1-u} \right) - \left(\frac{v}{1-v} \right) \right] \times \left[\left(\frac{u}{1-u} \right) + \left(\frac{u}{1-v} \right) \right]^{-1} \right| \times P \left(\frac{u}{1-u}, \frac{v}{1-v} \right) \times \frac{dudv}{(1-u)^2(1-v)^2} \right], \quad (12)$$

Table 2. Values of $[_B R_1(y)]_t$ and $[_B R_1(z)]_t$ as functions of σ_A and y_t for the non-centrosymmetric case

σ_A ↓	$[_B R_1(y)]_t$					$[_B R_1(z)]_t$					
	$y_t \rightarrow$	0.00	0.15	0.30	0.45	0.60	$y_t \rightarrow$	0.00	0.15	0.30	0.45
0.000	42.920	41.074	37.096	32.931	29.740	100.000	97.800	91.774	83.442	74.733	
0.040	42.852	41.008	37.037	32.881	29.696	99.840	97.647	91.639	83.333	74.647	
0.080	42.784	40.812	36.863	32.731	29.564	99.360	97.188	91.236	83.003	74.387	
0.120	42.703	40.485	36.574	32.482	29.345	98.560	96.323	90.564	82.452	73.951	
0.160	41.826	40.030	36.171	32.137	29.041	97.440	95.351	89.620	81.677	73.337	
0.200	41.216	39.449	35.557	31.695	28.654	96.000	93.972	88.404	80.676	72.540	
0.240	40.475	38.743	35.033	31.161	28.184	94.240	92.285	86.914	79.444	71.553	
0.280	39.606	37.916	34.301	30.534	27.635	92.160	90.290	85.146	77.976	70.371	
0.320	38.612	36.969	33.465	29.819	27.007	89.760	87.985	83.098	76.266	68.985	
0.360	37.493	35.904	32.525	29.014	26.302	87.040	85.371	80.766	74.307	67.305	
0.400	36.251	34.727	31.489	28.122	25.520	84.000	82.444	78.146	72.092	65.261	
0.440	34.886	33.424	30.337	27.142	24.659	82.360	80.864	76.126	70.885	64.360	
0.460	34.157	32.731	29.725	26.618	24.198	80.640	79.206	75.233	69.611	63.000	
0.480	33.397	32.008	29.087	26.071	23.717	78.840	77.468	73.665	68.269	62.376	
0.500	32.606	31.255	28.423	25.501	23.215	76.960	75.653	72.022	66.856	61.008	
0.520	31.783	30.472	27.731	24.907	22.691	75.000	73.758	70.303	65.372	59.935	
0.540	30.929	29.658	27.012	24.390	22.144	72.960	71.784	68.508	63.815	58.613	
0.560	30.049	28.813	26.285	23.829	21.574	70.840	69.731	66.635	62.143	57.151	
0.580	29.117	27.936	25.488	23.227	20.979	68.640	67.598	64.658	60.458	55.757	
0.600	28.161	27.026	24.682	22.578	20.359	66.360	65.386	62.655	58.094	54.218	
0.610	27.670	26.558	24.267	22.1918	19.7038	64.000	63.093	60.545	56.822	52.603	
0.620	27.170	26.082	23.845	21.752	19.0331	62.790	61.917	59.460	55.870	51.766	
0.630	26.661	25.598	23.415	21.359	18.3577	61.560	60.720	58.355	54.889	50.909	
0.640	26.143	25.104	22.979	20.919	17.6774	60.310	59.504	57.242	53.886	50.031	
0.650	25.616	24.602	22.530	20.477	17.0000	59.040	58.273	56.110	52.813	49.133	
0.660	25.079	24.091	22.075	20.012	16.3331	57.750	57.016	54.916	51.819	48.214	
0.670	24.533	23.570	21.612	19.607	15.6887	56.440	55.733	53.729	50.873	47.273	
0.680	23.977	23.041	21.139	19.194	15.0694	55.110	54.436	52.520	49.987	46.311	
0.690	23.412	22.501	20.658	18.772	14.4744	53.760	53.118	51.290	49.158	45.327	
0.700	22.836	21.953	20.169	18.335	13.9029	52.390	51.780	50.040	48.387	44.321	
0.710	22.251	21.397	19.669	17.883	13.3547	51.000	50.427	48.776	47.654	43.292	
0.720	21.655	20.826	19.161	17.455	12.8277	49.590	49.043	47.160	46.909	42.241	
0.730	21.049	20.247	18.643	16.998	12.3200	48.160	47.644	46.160	46.160	41.164	
0.740	20.432	19.659	18.115	16.553	11.8311	46.710	46.224	44.823	44.660	40.065	
0.750	19.805	19.059	17.577	16.055	11.3604	45.240	44.784	43.465	43.280	38.942	
0.760	19.166	18.450	17.029	15.568	10.9077	43.750	43.323	42.084	42.084	37.795	
0.770	18.517	17.829	16.471	15.071	10.4729	42.240	41.841	40.682	40.682	36.622	
0.780	17.857	17.198	15.902	14.563	10.0563	40.710	40.339	39.257	39.257	35.425	
0.790	17.185	16.556	15.322	14.045	9.6577	39.160	38.817	37.810	37.810	34.204	
0.800	16.501	15.902	14.731	13.516	9.2760	37.590	37.273	36.341	36.341	32.953	
0.810	15.806	15.237	14.129	12.975	8.9113	36.000	35.709	34.849	34.849	31.678	
0.820	15.098	14.560	13.516	12.422	8.5636	34.390	34.124	33.334	33.334	30.376	
0.830	14.379	13.871	12.890	11.857	8.2329	32.760	32.518	31.796	31.796	29.047	
0.840	13.647	13.170	12.252	11.280	7.9184	31.110	30.892	30.235	30.235	27.690	
0.850	12.907	12.456	11.602	10.689	7.6196	29.440	29.440	28.650	28.650	26.305	
0.860	12.162	11.730	10.939	10.086	7.3366	27.750	27.750	27.042	27.042	24.892	
0.870	11.413	10.991	10.263	9.469	7.0692	26.040	26.040	25.411	25.411	23.451	
0.880	10.659	10.239	9.573	8.838	6.8174	24.310	24.310	23.756	23.756	22.000	
0.890	9.905	9.474	8.870	8.192	6.5807	22.560	22.560	22.077	22.077	20.549	
0.900	9.151	8.714	8.151	7.531	6.3495	20.790	20.691	20.373	20.373	19.098	
0.910	8.397	8.001	7.487	6.858	6.1242	19.000	18.917	18.646	18.646	17.744	
0.920	7.643	7.291	6.817	6.179	5.9050	17.190	17.117	16.894	16.894	16.387	
0.930	6.889	6.588	6.151	5.494	5.6919	15.360	15.297	15.126	15.126	14.662	
0.940	6.135	5.878	5.478	4.810	5.4849	13.510	13.456	13.278	13.278	12.856	
0.950	5.381	5.169	4.809	4.126	5.2839	11.640	11.594	11.400	11.400	11.019	
0.960	4.627	4.458	4.130	3.442	5.0889	9.750	9.712	9.508	9.508	9.148	
0.970	3.873	3.748	3.461	2.758	4.9000	7.840	7.811	7.604	7.604	7.273	
0.980	3.119	3.037	2.791	2.074	4.7171	5.910	5.886	5.704	5.704	5.394	
0.990	2.365	2.321	2.117	1.390	4.5402	3.960	3.941	3.800	3.800	3.514	
1.000	1.611	1.600	1.433	0.706	4.3693	2.000	1.993	1.900	1.900	1.640	

where $R_1^f(y)$ is known to be (Parthasarathi & Parthasarathy, 1977; hereafter PP, 1977)

$$R_1^f(y) = 2 - \frac{2}{\sigma_B} \ln(1 + \sigma_B). \tag{13}$$

Index $[R_1^f(z)]_t$. Equation (40) of part I is valid for this case as well. In this case the final expression can be shown to be

$$[R_1^f(z)]_t = \frac{1}{\beta_{NC}} \left[R_1^f(z) - 2 \int_0^{y/(1+y)} \int_0^1 \left| \left[\left(\frac{u}{1-u} \right)^2 - \left(\frac{v}{1-v} \right)^2 \right] \right| \right]$$

$$\times \left[\left(\frac{u}{1-u} \right)^2 + \left(\frac{v}{1-v} \right)^2 \right]^{-1} \times P \left(\frac{u}{1-u}, \frac{v}{1-v} \right) \frac{du dv}{(1-u)^2(1-v)^2}, \tag{14}$$

where $R_1^f(z)$ is known to be (PP, 1977)

$$R_1^f(z) = 2\sigma_B/(1 + \sigma_B). \tag{15}$$

3. Discussion of the theoretical results

The theoretical expression for the six different normalized R indices valid for truncated data have been derived in (4), (6), (8), (10), (12) and (14). As in the C case, these indices depend on the parameters y_1 and σ_A .

Table 3. Values of $[R_1^f(y)]_t$ and $[R_1^f(z)]_t$ as functions of σ_A and y_1 for the non-centrosymmetric case

σ_A	$[R_1^f(y)]_t$					$[R_1^f(z)]_t$				
	$y_1 \rightarrow 0.00$	0.15	0.30	0.45	0.60	$y_1 \rightarrow 0.00$	0.15	0.30	0.45	0.60
0.000	61.371	59.387	56.213	53.963	53.376	100.000	98.071	94.184	90.855	89.518
0.040	61.340	59.356	56.183	53.934	53.347	99.960	98.030	94.144	90.813	89.479
0.080	61.247	59.263	56.093	53.847	53.259	99.839	97.908	94.022	90.694	89.359
0.120	61.091	59.107	55.942	53.702	53.111	99.637	97.704	93.817	90.495	89.158
0.160	60.871	58.887	55.729	53.497	52.902	99.352	97.414	93.552	90.213	88.873
0.200	60.599	58.603	55.453	53.230	52.631	98.980	97.037	93.152	89.856	88.502
0.240	59.803	57.821	54.691	52.503	51.888	98.517	96.569	92.685	89.379	88.040
0.280	59.301	57.319	54.210	52.035	51.409	97.959	96.004	92.122	88.839	87.483
0.320	58.718	56.737	53.647	51.492	50.851	97.300	95.337	91.457	88.109	86.823
0.360	58.047	56.068	53.000	50.868	50.209	96.531	94.559	90.682	87.432	86.251
0.400	57.283	55.305	52.263	50.156	49.473	95.644	93.661	89.789	86.550	85.415
0.440	56.462	54.483	51.423	49.364	48.597	94.626	92.631	88.765	85.530	84.444
0.480	55.593	53.613	50.568	48.529	47.747	93.463	91.454	87.596	84.410	83.321
0.500	55.430	53.458	50.481	48.430	47.678	92.820	90.805	86.951	83.776	82.685
0.520	55.489	53.517	50.540	48.489	47.737	92.135	90.112	86.264	83.144	82.053
0.540	55.616	53.644	50.667	48.616	47.864	91.403	89.372	85.530	82.370	81.279
0.560	55.804	53.832	50.855	48.805	48.053	90.620	88.589	84.747	81.583	80.492
0.580	56.047	54.075	51.093	49.043	48.291	89.784	87.757	83.916	80.750	79.659
0.600	56.336	54.364	51.381	49.332	48.580	88.889	86.863	83.015	79.845	78.754
0.620	56.670	54.700	51.716	49.667	48.917	87.930	85.865	82.058	78.965	77.874
0.638	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.640	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.650	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.660	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.670	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.680	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.690	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.700	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.710	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.720	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.730	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.740	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.750	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.760	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.770	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.780	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.790	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.800	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.810	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.820	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.830	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.840	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.850	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.860	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.870	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.880	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.890	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.900	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.905	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.910	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.915	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.920	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.925	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.930	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.935	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.940	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.945	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.950	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.955	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.960	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.965	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.970	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.975	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.980	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.985	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.990	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
0.995	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000
1.000	57.000	55.030	52.050	49.999	49.249	87.000	85.000	81.200	78.100	77.000

The variation of these indices as a function of y_t for the situation $\langle |\Delta \mathbf{r}| \rangle = 0.2 \text{ \AA}$ and $\sin \theta/\lambda = 0.4 \text{ \AA}^{-1}$ is shown in Fig. 1(a)–(f). A study of these figures shows that, in the *NC* case, as y_t increases, $[R]_t$ decreases. This decrease is much less when y_t is small (say $y_t < 0.15$) and becomes more pronounced for larger y_t . This behaviour of $[R]_t$ in the *NC* case may be contrasted with its behaviour in the *C* case (see Fig. 1 of part I). The evaluation of the overall values of the *R* indices for the *NC* case is quite analogous to that described in part I for the *C* case. The values of $[R]_t$ (in percent) as

functions of σ_A and y_t required for the evaluation of $[R]_t$ are given in Tables 1–3 for the various *R* indices.

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Absorption Coefficients of Electrons in Crystals

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Abstract

Absorption coefficients of Si, Ge and InSb are obtained from the analysis of extinction contours in the acceleration voltages ranging from 100 to 750 kV. The cross sections of thermal diffuse scattering, plasmon excitation and electronic excitation are obtained separately. An agreement between theory and experiment is obtained for thermal diffuse scattering and plasmon scattering. The theoretical estimation based on the electron gas statistical model is favourable for the electronic excitation.

1. Introduction

Since the mean and anomalous absorption coefficients are important parameters for electron diffraction and microscopy, many investigations have been carried out experimentally and theoretically. Early attempts to measure absorption coefficients were made on ordinary electron micrographs (Kohra & Watanabe, 1959; Hashimoto, 1964). In these cases some of the inelastic scattering was included in the pattern. It was pointed out, however, that the elastic intensity of the extinction contour of the electron microscopic image did not agree with the theoretical one (Ichimiya, 1969; Takagi & Ishida, 1970). The discrepancy between theory and

experiment was shown to be mainly due to technical problems (Kamiya & Gotō, 1980). The aim of the present paper is to extend the experiment to the case of higher accelerating voltages by using electron micrographs. The diffraction pattern was also used for the measurement of absorption coefficients (Molière & Lehmpfuhl, 1961) and later Meyer-Ehmsen (1969) measured them from transmitted and diffracted intensities of elastic scattering at an accelerating voltage of ~50–70 kV. The present results agree quite well with that given by Meyer-Ehmsen. The result also shows that the cross sections due to plasmon excitation and thermal diffuse scattering agree fairly well with theories by Ashley & Ritchie (1970) and Hall & Hirsch (1965), and that the cross section due to electronic excitation agrees with the theory of Ritchie & Howie (1977).

2. Experiments

Experiments were made in the cases of Si, Ge and InSb at several accelerating voltages between 100 and 750 kV and at three different temperatures. The experimental procedure is the same as described previously (Kamiya & Gotō, 1980). The intensities of extinction contours formed by elastic scattering were obtained with a magnetic velocity analyzer (Ichinokawa, 1968; Kamiya, Shimizu & Suzuki, 1974). Most experiments were done at the Bragg position of the 220 reflection. The intensity of the extinction contour is analyzed by a method based on the two-beam approximation (Uyeda

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